

## Applying Fixed Box Model to Calculate the Temporal Variance of the Concentration of PM<sub>10</sub> in Thanh Xuan District, Hanoi (Vietnam)

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### Abstract

This report presents the initial research results of applying the Fixed Box Model to calculate the temporal variance of the concentration of particulate matter of 10 micrometers (PM<sub>10</sub>) one of the air pollutants that most commonly affects people's health. The input parameters (area source capacity of PM<sub>10</sub>, wind speed, mixing height, size of area source) were estimated based on the area source emission inventory results including: road source, mobile source, construction source, industry source and household domestic source in Thanh Xuan District. This emission inventory project was carried out from 9/2007 to 3/2008 by Hanoi Center for Environmental and Natural Resources Monitoring and Analysis (CENMA) and Research Center for Environmental Monitoring and Modeling (CEMM) - Hanoi University of Science, of which, CEMM played a consultative role. The project was sponsored by the Swiss - Vietnamese Clean Air Program (SVCAP). The results show that:

- The graph describing the temporal variance of the concentration of PM<sub>10</sub> has an exponential function, rising gradually until it reaches a saturated state.
- Concentration of PM<sub>10</sub> C(t) is in inverse proportion to wind speed (U) and mixing height (H) at a fixed box length (L) and area source capacity (M<sub>s</sub>).
- There exists a specific time constant  $\tau$  for life time of pollutants in each case.
- The results from the Fixed Box Model are verified by real data get high accuracy.

**Keywords:** *Particulate Matter, Fixed Box Model, Emission Inventory*

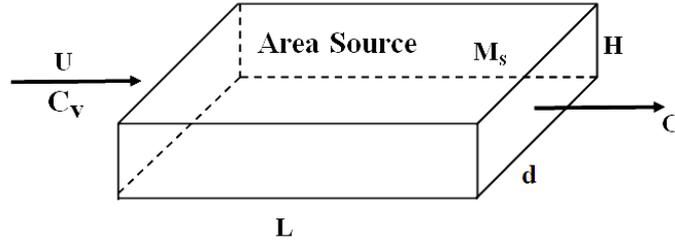
### 1. Theoretical background of the Fixed Box Model

(P.N.Ho, V.V. Manh *et al.* 2005, P.N.Ho, D.N.Bach 2006)

Area source is the set of emission sources in a large area unit such as the toxic vapor dispersion from transportation activities, manufactures, households' cooking activities, dust from coal and sand banks, etc. If an area source is created from some point sources which are not very large, mathematical models can be used to calculate for each point source and then their results will be aggregated to infer the concentrations of pollutants at the investigated points. Also, the surface area can be divided into a set of parallel road sources. Calculating formulas will be used for each road source and their results will also be aggregated. Besides the above methods, we can also use a fixed box model in order to estimate the level of atmospheric pollution caused by area sources (districts, cities, mine areas, etc.). The advantage of the fixed box model in comparison with the dispersion models of point sources and line sources is able to solve a non steady state problem. Its content is as follows:

Assuming that the air block at the studied area has a parallelepiped shape with length L(m), width d(m), and height H(m) which is often the height of atmospheric turbulent mixing layer. Capacity of area source

is  $M_s$  ( $\text{mg}/\text{m}^2 \cdot \text{s}$ ); the wind whose direction is perpendicular to the width has the average speed  $U$  ( $\text{m}/\text{s}$ ); the wind takes a pollution flow which has the concentration  $C_v$  ( $\text{mg}/\text{m}^3$ ); the concentration inside the parallelepiped is equal  $C$  ( $\text{mg}/\text{m}^3$ ) (see figure 1.1):



**Figure 1.1. Parallelepiped characterizing the air block at the studied area**

Suppose that pollutants do not diffuse through 2 boundary slices parallel with wind direction as well as with top and bottom slices, it will create the identical average concentration of pollutants in the air box. According to the law of mass balance, we must have:

$$LdH \frac{\partial C}{\partial t} = M_s Ld + dHuC_v - dHuC \quad (1.1)$$

It means that: the variation speed of pollutants in the box = total of pollution level inside the box – pollution level going out of the box.

If the time span is infinite ( $t \rightarrow \infty$ ) the variation of pollutant reaches the stable equilibrium:  $\frac{\partial C}{\partial t} = 0$

(steady state), from the equation (1.1) we have:  $C_\infty = \frac{M_s L}{uH} + C_v$  (1.2)

From the equation (1.2) it can be found that if the air going inside the box is clean ( $C_v=0$ ) the stable pollutant concentration will be in direct ratio to the capacity of emission source  $M_s$  and in reverse ratio to coefficient  $uH$ . If wind flows takes pollutants with it ( $C_v \neq 0$ ) then the effect of wind, which increases the pollutants in the parallelepiped, must be added in.

In case of transient state:  $\frac{\partial C}{\partial t} \neq 0$

Considering  $C_0$  as the concentration of pollutant in the air box at the studied area at the time  $t=0$ , solving the differential equation (1.1) we will have the following result:

$$C(t) = \left( \frac{M_s L}{uH} + C_v \right) \left( 1 - e^{-\frac{ut}{L}} \right) + C_0 e^{-\frac{ut}{L}} \quad (1.3)$$

If wind flow blows into the box does not take pollutants with it and  $C_0=0$ , the equation (1.3) becomes:

$$C(t) = \frac{M_s L}{uH} \left( 1 - e^{-\frac{ut}{L}} \right) \quad (1.4)$$

When  $t = \tau = L/u$  is called time constant, which characterizes the residual time of pollutant in the box, the formula (1.4) becomes:

$$C(u) = \frac{M_s L}{euH} (e - 1) \quad (1.5)$$

## 2. Calculation

### 2.1 Calculating the input parameters of the model based on the real data of emission inventory in Thanh Xuan District

(P.N.Ho, V.V. Manh *et al.* 2007, CENMA 2008)

#### 2.1.1 Dimension of the box

Length L (maximum): 5310 m; Width d (maximum): 3130 m

#### 2.1.2 Calculating the capacity of area source Ms of PM<sub>10</sub>

Area sources in this case are the emission sources such as road sources (42 roads), mobile sources (emission from vehicles on 42 roads), construction sources (4 areas of civil construction and construction of 105 households), emission sources from manufactures (22 sources) and household domestic sources (47094 households).

##### 2.1.2.1 Calculating the emission capacity of PM<sub>10</sub> from road sources

- Emission of PM<sub>10</sub> from a type of vehicles on road is calculated according to the following formula:

$$M_{PM10} = (Ef \times \text{Sum of VKT} \times 365) / 1000000 \quad (\text{ton/year}) \quad (2.1)$$

- VKT (Vehicles Kilometers Traveled) is the number of km which vehicle travels in one day;
- Ef: is the road emission coefficient of PM<sub>10</sub> emitted by each vehicle (g/km).

In which:  $Ef = k(sL/2)0.65(W/3)1.5(1-P/4N)$  (AP42, EPA, 1999).

- k: coefficient considering the dimension of PM (g/km); sL: quantity of alluvia on the road surface (g/m<sup>2</sup>) varying from 0 - 300g/m<sup>2</sup>; W: average weight of vehicle (ton); P: total rainy days in year; N: number of days in year, N=365 days.

The concretely calculated parameters are in the following table:

Vehicle type	4-16 places	24 places and over	Lorry	Container truck	Bus	Motorbike
W (ton)	3	5	5	25	10	0.12

k (PM <sub>10</sub> )	sL	P	N
4.6	10,20,30	86	365

**Table 2.1. Parameters of vehicle and parameters related to road source**

- The emission capacity of PM<sub>10</sub> from road sources in Thanh Xuan District (calculating for all of 42 roads in Thanh Xuan District) is estimated as follows: 2438.88 (tons/year).

##### 2.1.2.2 Calculating the emission capacity of PM<sub>10</sub> from mobile sources

- Emission of PM<sub>10</sub> from exhaust of vehicle is calculated according to the formula (2.1), in which:
- Ef: is emission coefficient of PM<sub>10</sub> caused by exhaust of each type of vehicle, given in table 2.2.
- The emission capacity of PM<sub>10</sub> from mobile sources in Thanh Xuan District (calculating for all of 42 roads in Thanh Xuan District) is estimated as follows: 148,79 (tons/year).

Vehicle types	Emission coefficient of PM <sub>10</sub> (g/km)
4-16 places	0.10
24 places and over	0.15
Lorry	0.23
Container truck	3.28
Bus	1.97
Motorbike	0.10

**Table 2.2. Emission coefficient of PM<sub>10</sub> from mobile sources (AP42)**

### 2.1.2.3 Calculating the emission capacity of PM<sub>10</sub> from construction sources

- Emission of PM<sub>10</sub> from construction activities is calculated according to the following formula:

$$M_{PM10} = S \times t \times E_f \quad (\text{ton/year}) \quad (2.2)$$

- S: The area of construction surface (m<sup>2</sup>); t: duration of construction (month/year); E<sub>f</sub>: emission coefficient = 0.025 kg/m<sup>2</sup>.month (AP42)

- The emission capacity of PM<sub>10</sub> from construction activities in Thanh Xuan District (including 4 concentrated civil construction areas and individual construction of 105 households) is as follows: 299.93 (tons/year).

### 2.1.2.4 Calculating the emission capacity of PM<sub>10</sub> from domestic cooking activities

- Emission of PM<sub>10</sub> from domestic cooking activities is calculated according to the following formula:

$$M_{PM10} = \text{Mass of fuel used} \times \text{Emission coefficient } E_f \quad (\text{ton/year}) \quad (2.3)$$

- Emission coefficient from coal burning: E<sub>f</sub> = 2.32 kg/ton ; Emission coefficient from gas burning: E<sub>f</sub> = 0.0001 kg/ton

- The emission capacity of PM<sub>10</sub> from domestic cooking activities in Thanh Xuan District (47094 households) is as follows: 45.11 (ton/year).

### 2.1.2.5 Calculating the emission capacity of PM<sub>10</sub> from point sources

The formula of calculating the emission capacity of PM<sub>10</sub> from small point sources:

- If the fuel used is coal:

$$M_{PM10} = \text{Fuel amount} \times \text{Emission coefficient } E_f \times \text{ash coefficient of coal} \quad (\text{ton/year}) \quad (2.4)$$

E<sub>f</sub> = 0.357 kg/ton;

Ash coefficient of coal: 3.125 kg/ton

- If the fuel used is petroleum and gas, the formula (2.3) can be used to calculate, in which: E<sub>f</sub> = 0.2 kg/m<sup>3</sup> for petroleum and E<sub>f</sub> = 0.000027053 kg/ton for gas; E<sub>f</sub> coefficients in formulas (2.3) - (2.4) come from (AP42, PREIS 2004)

- The emission capacity of PM<sub>10</sub> from small point sources in Thanh Xuan District (22 manufactures) is as follows: 20.14 (ton/year).

## 2.2 Adjustment of the calculated results of emission capacity in the studied area

At present, there is no standard emission coefficient for the above types of studied sources in Vietnam, United States emission coefficients (according to the document AP-42, EPA and PUNE project, India, 2004) (PREIS 2004) were used during the calculating process. Therefore, it is necessary to adjust the calculated results in order to obtain a relative accuracy. The adjustment principle is based on the surveys of each specific source to correct and estimate the emission capacity  $M$  for the studied area, the results are showed in table 2.3:

Emission sources	Calculated capacity $M^*$ according to document AP-42 and PUNE (ton/year)	Adjustment coefficient (d)	Adjusted capacity (ton/year) $M = M^* (d+1)$
	<b>PM<sub>10</sub></b>		<b>PM<sub>10</sub></b>
Household construction	179	0.2	214.8
Civil construction	120.93	0.3	157.21
Domestic cooking	45.11	0.15	51.88
Road source	2438.88	0.35	3292.49
Mobile source	148.79	0.15	171.11
Manufacture	20.14	0.2	24.17
<b>Total</b>	<b>2952.85</b>		<b>3911.65</b>

**Table 2.3. Estimation of emission capacities of PM<sub>10</sub>, from emission sources in Thanh Xuan District in 2007 with the adjustment coefficient d**

## 2.3 Calculation Scenarios

### 2.3.1 The input parameters of fixed box model based on the table 2.3

- Emission capacity of area source  $M_s = 0.0136 \text{ mg/m}^2 \text{ s}$  ;
- The length of the box: = 5310 m;      - The width of the box = 3130 m
- Mixing height:  $H_1 = 120 \text{ m}$ ;  $H_2 = 200 \text{ m}$

Mixing height is the height  $H$  in the atmospheric boundary layer where the turbulent coefficient  $A_z = KZ\zeta = \text{const}$  with  $z > H$ ; Of which,  $K_z$  is the vertical turbulent coefficient,  $\zeta$  is the average density of the studied atmospheric layer.

The researches of Obukhov and Budyko (L.D.Quang, P.N.Ho 2006) showed that Profile of  $A_z$  (or turbulent coefficient  $K_z$ ) in the atmospheric border layer has a linear dependence on the distance of vertical movement of turbulent cycle  $l_z = \chi z$  ( $\chi$ - Karman constant  $\approx 0.4$ ) in the equilibrium condition to the height  $H = l_{z\text{max}}$ , corresponding with the height  $Z_{\text{max}}$  varying from 300-500m. Therefore, the height  $H$  can be estimated varies from 120-200m.

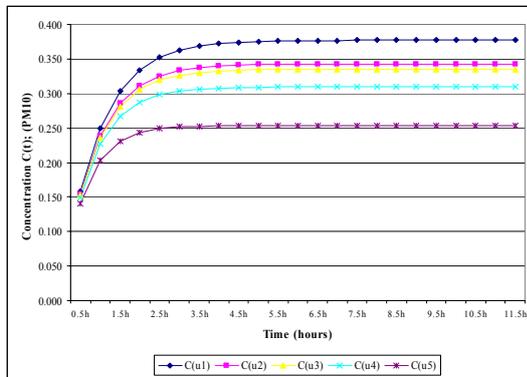
- Wind speed: wind speed and frequency are shown in the table 2.4.

No.	Wind direction	Annual average speed (m/s)	Wind frequency (%)
1	North	1.95	22.62
2	Northern East	2.38	34.95
3	East	1.60	26.68
4	Southern East	1.76	51.2
5	Northern West	1.8	14.21

Table 2.4. The wind regime in the area of Hanoi in 2007 (Lang station)

### 2.3.2 Calculated results

Case 1: with  $H_1 = 120$  m:



Case 2: with  $H_2 = 200$  m:

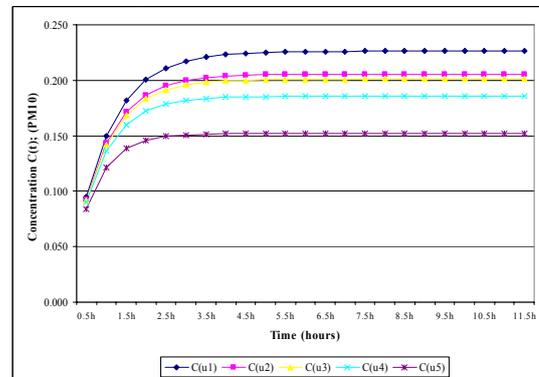


Figure 2.1. Temporal variance of  $PM_{10}$

	$u_1 = 1.6$ m/s	$u_2 = 1.76$ m/s	$u_3 = 1.8$ m/s	$u_4 = 1.95$ m/s	$u_5 = 2.38$ m/s
$\tau$ (minute)	55.31	50.28	49.17	45.38	37.18
$C(mg/m^3); PM_{10}$	0.238	0.217	0.212	0.196	0.160

Table 2.5. Calculated results of pollutant concentration (C) corresponding to the residual time  $\tau$  and the change of wind speed ( $H_1=120$ m)

	$u_1 = 1.6$ m/s	$u_2 = 1.76$ m/s	$u_3 = 1.8$ m/s	$u_4 = 1.95$ m/s	$u_5 = 2.38$ m/s
$\tau$ (minute)	55.31	50.28	49.17	45.38	37.18
$C(mg/m^3); PM_{10}$	0.143	0.130	0.127	0.117	0.096

Table 2.6. Calculated results of pollutant concentration (C) corresponding to the residual time  $\tau$  and the change of wind speed ( $H_2=200$ m)

Parameter	$u_5 = 2.38 \text{ m/s}$		$u_1 = 1.6 \text{ m/s}$	
	$t_{\infty}(\text{h})$	$C_{\max} (\text{mg/m}^3)$	$t_{\infty}(\text{h})$	$C_{\max} (\text{mg/m}^3)$
PM <sub>10</sub>	3.5	0.253	6.5	0.377

**Table 2.7. Calculated results of concentration  $C_{\max}$  corresponding to the time of starting saturation  $t_{\infty}$  of pollutants in the case of  $H_1=120\text{m}$**

Parameter	$u_5 = 2.38 \text{ m/s}$		$u_1 = 1.6 \text{ m/s}$	
	$t_{\infty}(\text{h})$	$C_{\max} (\text{mg/m}^3)$	$t_{\infty}(\text{h})$	$C_{\max} (\text{mg/m}^3)$
PM <sub>10</sub>	3.5	0.152	5.5	0.226

**Table 2.8. Calculated results of concentration  $C_{\max}$  corresponding to the time of starting saturation  $t_{\infty}$  of pollutants in the case of  $H_2=200\text{m}$**

In order to verify the calculated result of the model with the measured data, the measured data of PM<sub>10</sub> at 3 points (50 Khuong Dinh – Thuong Dinh ; D<sub>4</sub> collective quarter VACVINA-Nhan Chinh and A<sub>11</sub>- north of Thanh Xuan) in Thanh Xuan District together with the data of the emission inventory during 3 continuous days from 28-30/11/2007 have been used. The time of sampling: 4 times per day at 1h, 7h, 13h, 19h; the duration of sampling is 1h for each time, the measured data were averaged for each time, after that they were averaged for all of 4 times to get the specific values for 24h; and the value of concentration  $C_{\max}$  from the saturate curves at  $t_{\infty}$  is considered as the average concentration of 24h which is taken to compare, the results are indicated in the table 2.9.

Parameter	Measured concentration ( $u = 2,2 \text{ m/s}$ )	Calculated concentration of the model ( $H_1= 120\text{m}; u = 2,38\text{m/s}$ )	Relative error (%)	Measured concentration ( $u = 2,2 \text{ m/s}$ )	Calculated concentration of the model ( $H_2= 200\text{m}; u = 2,38\text{m/s}$ )	Relative error (%)
PM <sub>10</sub>	0,259	0,253	2,4	0,259	0,152	41,4

**Table 2.9. Comparison between the calculated result of the model and the measured result ( $\text{mg/m}^3$ )**

Table 2.9 shows that: the calculated result is closer to the measured result when  $H_1 < H_2$ . Therefore, the estimation of mixing height suitable with the actual conditions plays an important role.

- The calculated results from the model that were smaller than the measured results corresponds with the physical significance because the measured concentration at the monitoring point is :  $C_d = C_n + C_t + C_o$ , of which:  $C_n$  is the existing foundation concentration,  $C_t$  is the calculated concentration of emission from area sources and  $C_o$  is the concentration generated by wind flow which takes pollutants from other areas into the box (this element has not been considered yet in the research).

- The calculated results from the model also indicate that there has been a scientific basis for the adjustment in emission inventory and the adjustment has obtained an acceptable accurate level.

### 3. Conclusions

- The above figures show that all of the lines of concentration of pollutant PM<sub>10</sub> varying with time (corresponding to various wind speeds and mixing height) have the shape of exponential function, gradually increasing with time until a value  $t_{\infty}$  where the concentration reaches the saturation (the graph is parallel with the horizontal axis);

- The higher the wind speed is, the shorter the time of reaching saturation is. For example: in the case of calculating for  $u_5 = 2,38$  m/s and  $H_1 = 120$  m, the time for reaching the saturation state of  $PM_{10}$  is after 3,5 hours;
- Pollutant's concentration  $C(t)$  is in reverse ratio to wind speed  $U$  and mixing height  $H$  corresponding to the fixed box length  $L$  and area source capacity  $M_s$ ;
- Defined the time constant  $\tau$ , characterizing the residual duration of  $PM_{10}$  in the box corresponding to each studied case. The higher the wind speed is, the shorter the residual duration of pollutant is; With the wind speed varying from 1,6 – 2,38 m/s, the residual time  $\tau$  of pollutant in the box is 55,31 - 37,18 minutes;
- Compared with the Vietnamese standard TCVN 5937-2005 (24h average), the concentration of  $PM_{10}$  is 1,6-2,5 times higher than the standard (in the case of wind speed 2,38 – 1,6m/s and mixing height  $H_1=120$ m). In the case of mixing height  $H_2=200$ m and wind speed = 1,6 m/s, the concentration of  $PM_{10}$  is 1,5 time higher than the Vietnamese standard.
- The calculated results from the model which were verified by the measured data indicated that the estimation of mixing height  $H = 120$ m gives the calculated result closer to the measured result;
- The initial result may have significance for studying the application of this fixed box model on evaluating the air quality in districts of Hanoi city in particular and urban areas of Vietnam in general.

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